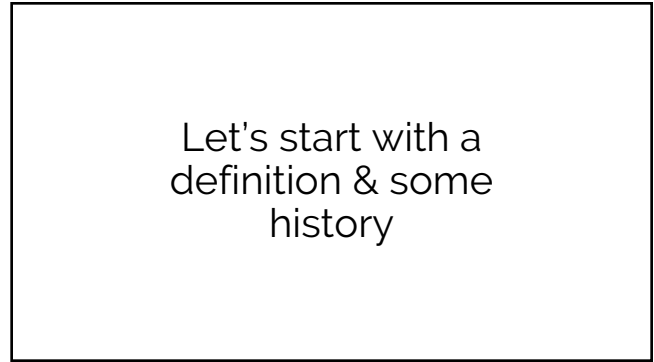




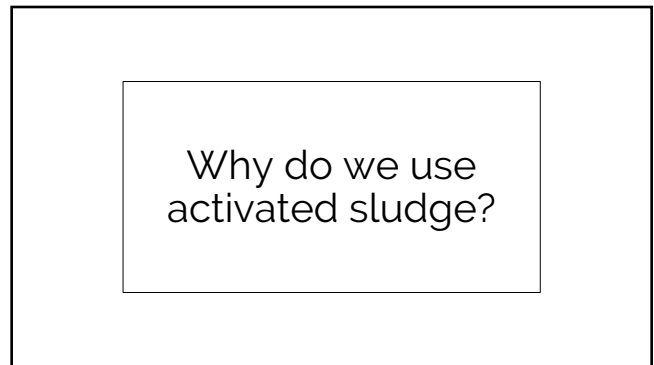
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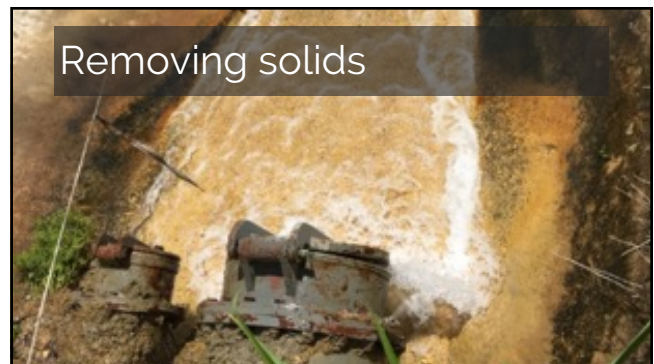
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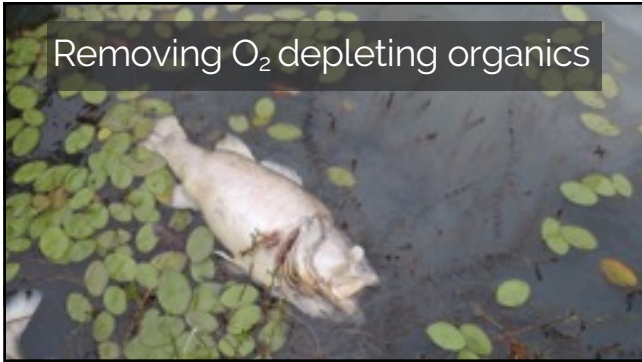
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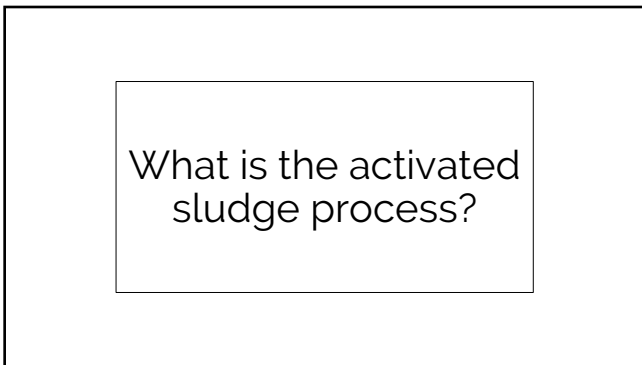
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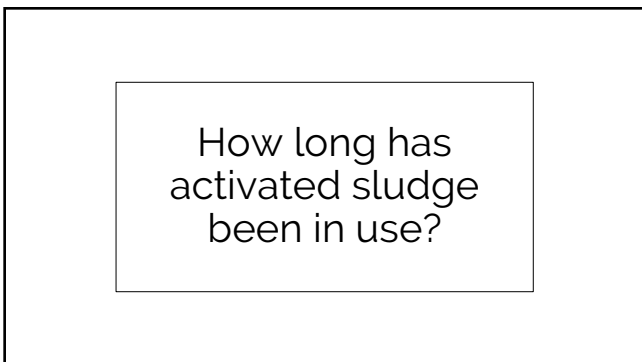
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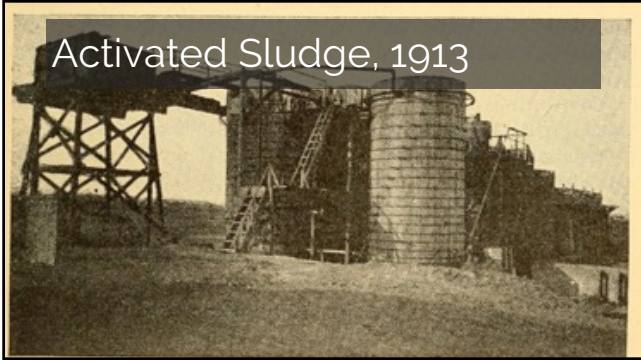
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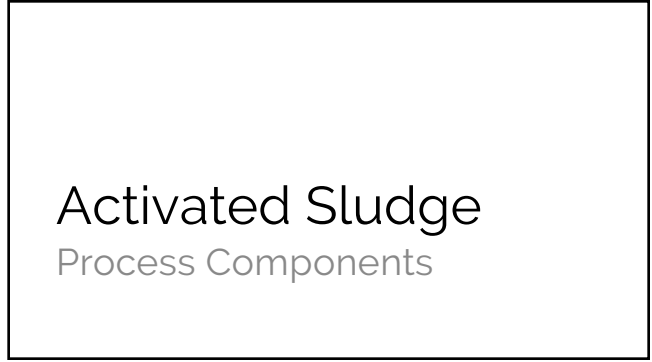
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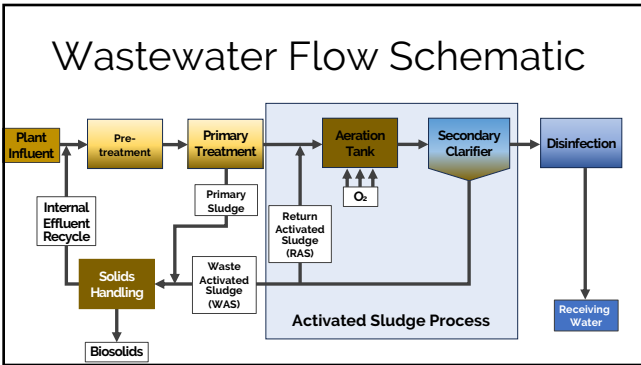
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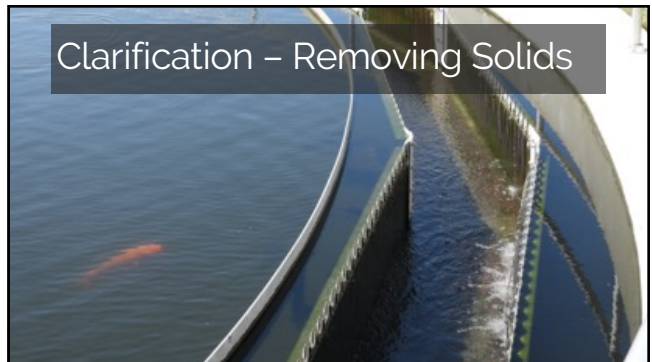
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22

Activated Sludge

Biological Components

23

Aerobic Bacteria

- Need oxygen
- Grow relatively fast
- Produce little to no odor
- Are efficient waste oxidizers

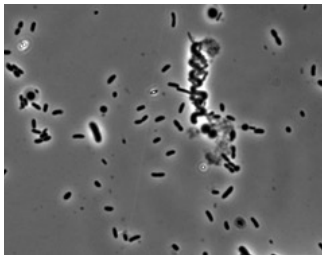



Image Source: <http://ofbacteriaandmen.blogspot.com/2013/02/bacteria-in-wastewater-treatment-plant.html>

24

Facultative Bacteria


- Don't need oxygen (but typically prefer it)
- Grow slower than aerobic microbes
- Produce unpleasant odors when oxygen is scarce
- Are less efficient waste oxidizers than aerobic microbes



1 μm

25

Filamentous Organisms



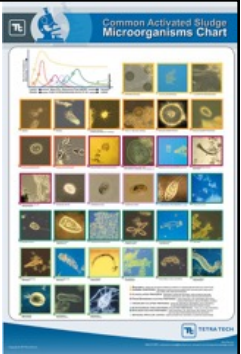
Nocardia Thiothrix Actinomycetes

- These **don't settle well** in secondary clarifiers, resulting in **poor effluent quality**
- Are often **minimized using chemicals** like bleach, polymer and flocculants

Image Source: <https://www.minsipu.com/india/ambrotment/temad/>

26

Other Organisms



Microscopic analysis of your system should be part of daily monitoring and process control

Usually correlate to plant performance

Indicator species will help you determine the health of the system and help predict where it's headed

Can be used as an early warning and to help prevent critical upsets

Can indicate sludge age and reflect recent high BOD loading

27



28

Bacterial Digestion

$$\begin{aligned}
 & \text{organic matter (wastewater)} \\
 & \quad + \text{O}_2 \\
 & \quad + \text{nutrients} \\
 & \quad + \text{microbes} \\
 \hline
 & = \text{new microbes} + \text{CO}_2 + \text{H}_2\text{O}
 \end{aligned}$$

29

Aerobic Oxidation: 3 perspectives

Bacterial standpoint: Food + Bacteria + O₂

Or

Operator standpoint: Waste + Activated Sludge + Aeration

Or

Chemical Reaction: Electron Donor + Energy + Reproduction + Electron Acceptor

End Products: = Oxidized Wastewater + More Bacteria + CO₂ + H₂O

30

BNR - Nutrient Removal

Nitrogen removal is a 2-step process:

- Nitrification (aerobic process) converts ammonia into nitrite and subsequently nitrate
- Denitrification (anoxic process) converts nitrate into nitrogen gas

Conventional BOD systems that run with longer aeration times often result in nitrification as well, but the denitrification process has to be separated from the aerobic step

31



32

Operational Variables

Influent BOD, DO, WAS

33



34



35



36



37



38

F/M Ratio: Food/Microorganisms

$$\frac{F}{M} = \frac{\text{total rate of applied food}}{\text{total microbe biomass}} = \frac{Q \times BOD}{V_{ab} \times MLVSS} = \left[\frac{\text{lb BOD}}{\text{lb VSS} \cdot \text{day}} \right]$$

Q = Flow Rate into aeration Tank
BOD = concentration of BOD in the flow into Aeration Tank
V_{ab} = volume of Aeration Tank
MLSS = concentration of suspended solids in the Aeration Tank
MLVSS (or VSS) = concentration of MLVSS in the Aeration Tank

Expressed as $\frac{\text{mass}}{\text{mass} \cdot \text{day}}$

39

F/M Ratio: Example

$$\frac{F}{M} = \frac{\text{total rate of applied food}}{\text{total microbe biomass}} = \frac{Q \times BOD}{V_{ab} \times MLVSS} = \left[\frac{\text{lb BOD}}{\text{lb VSS} \cdot \text{day}} \right]$$

Q = Flow Rate into aeration Tank
BOD = concentration of BOD in the flow into Aeration Tank
V_{ab} = volume of Aeration Tank
MLVSS = concentration of MLVSS in the Aeration Tank

$$\frac{F}{M} = \frac{Q \left[\frac{\text{Mgal}}{\text{day}} \right] \times BOD \left[\frac{\text{mg}}{\text{L}} \right] \times \frac{8.34 \text{ lb}}{\text{mg} \cdot \text{Mgal}}}{V_{ab} \left[\text{Mgal} \right] \times MLVSS \left[\frac{\text{mg}}{\text{L}} \right] \times \frac{8.34 \text{ lb}}{\text{mg} \cdot \text{Mgal}}} = \left[\frac{\text{lb BOD}}{\text{lb VSS} \cdot \text{day}} \right]$$

40

F/M Ratio: Calculate MLVSS

$$\frac{F}{M} = \frac{\text{total rate of applied food}}{\text{total microbe biomass}} = \frac{Q \times BOD}{V_{ab} \times MLVSS} = \left[\frac{\text{lb BOD}}{\text{lb VSS} \cdot \text{day}} \right]$$

Q = Flow Rate into aeration Tank
BOD = concentration of BOD in the flow into Aeration Tank
V_{ab} = volume of Aeration Tank
MLSS = concentration of suspended solids in the Aeration Tank
MLVSS (or VSS) = concentration of MLVSS (biomass) in the Aeration Tank

BOD - 200 mg/L 1) Calculate MLVSS: $MLVSS = 85\% \times MLSS \text{ concentration} = 85\% \times 2,400 \frac{\text{mg}}{\text{L}} = 2,040 \frac{\text{mg}}{\text{L}}$

Biomass - 85% of solids

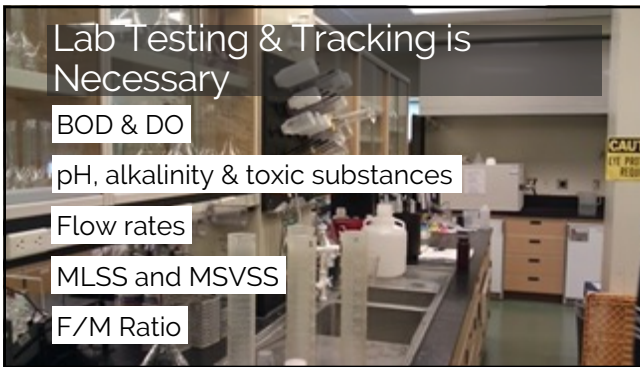
Tank Volume (V_{ab}) - 1 MG 2) Calculate F/M ratio:

Flow (Q) - 4 MG/day

MLSS - 2,400 mg/L

$$\frac{F}{M} = \left[\frac{\text{lb BOD}}{\text{lb VSS} \cdot \text{day}} \right] = \frac{Q \times BOD}{V_{ab} \times MLVSS} = \frac{4 \frac{\text{MG}}{\text{d}} \times 200 \frac{\text{mg}}{\text{L}}}{1 \text{ MG} \times 2,040 \frac{\text{mg}}{\text{L}}} = 0.4 \frac{\text{lb BOD}}{\text{lb VSS} \cdot \text{day}}$$

41



42

Typical ASP Lab Results

Test	Location	Common Range
COD	Influent	250 - 1,000 mg/L
	Primary Effluent	200 - 400 mg/L
	Final Effluent (Conv. ASP)	30 - 70 mg/L
BOD	Influent	150 - 400 mg/L
	Primary Effluent	100 - 280 mg/L
	Final Effluent (Conv. ASP)	10 - 20 mg/L
Suspended Solids	Influent	150 - 400 mg/L
	Primary Effluent	60 - 160 mg/L
	Mixed Liquor	1,000 - 4,500 mg/L
	Return Sludge	2,000 - 10,000 mg/L
	Final Effluent (Conv. ASP)	1 - 20 mg/L
Dissolved Oxygen (DO)	Mixed Liquor	0.5 - 4 mg/L
	Final Effluent (outfall)	2 - 6 mg/L

43

Typical ASP Loading Ranges

Loading Rate	Hydraulic Retention Time (hrs)	Sludge age (days)	Volumetric Loading (lb BOD/1000 ft ³)	F/M (lb/lb · day)
Low Rate	18-24	20 - 30	10 - 25	0.05 - 0.15
Conventional	6-8	5 - 15	20 - 40	0.2 - 0.5
High Rate	1-3	1 - 3	100 - 1,000	0.5 - 1.5

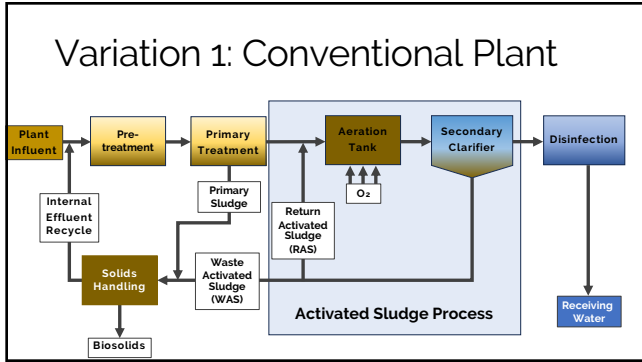
Source: Table 5.3 Operation of Wastewater Treatment Plants, Vol. 18th Edition, Water Programs, Sacramento State

44

Operation

Three Basic ASP Variations

45



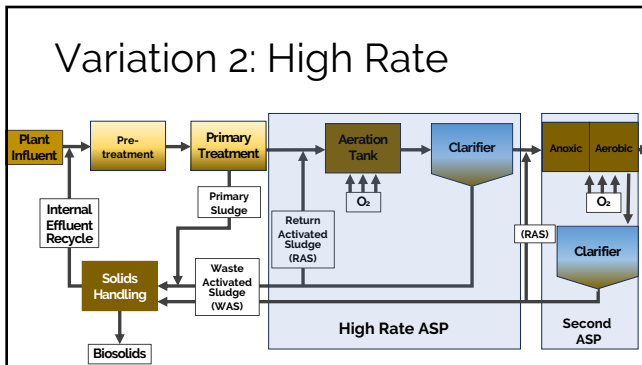
46

Variation 1: Conventional ASP

Loading Rate	Sludge age (days)	Volumetric Loading (lb BOD/1000 ft ³)	F/M (lb/lb · day)
Medium	5 - 15	20 - 40	0.2 - 0.5

Hydraulic retention time: 6-8 hours
 F/M Ratio: Moderate
 Organism Growth Rate: Slow
 Sludge Age: Mid-Range
 Effluent Quality: Good

47



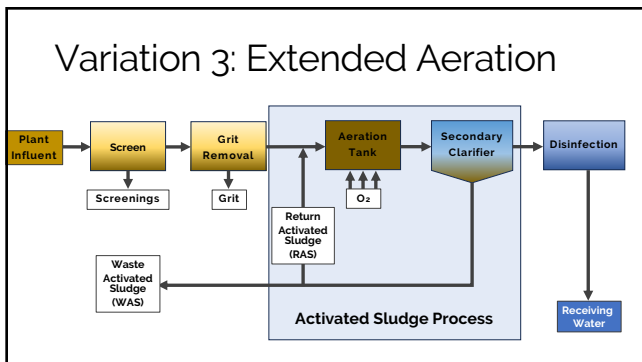
48

Variation 2: High Rate

Loading Rate	Sludge age (days)	Volumetric Loading (lb BOD/1000 ft ³)	F/M (lb/lb · day)
High Rate	1 - 3	100 - 1,000	0.5 - 1.5

Hydraulic Retention Time: 1-3 hours
 F/M Ratio: High
 Organism Growth Rate: High
 Sludge Age: Short
 Effluent Quality: Lower than desirable

49



50

Variation 3: Extended Aeration

Loading Rate	Sludge age (days)	Volumetric Loading (lb BOD/1000 ft ³)	F/M (lb/lb · day)
Low Rate	20 - 30	10 - 25	0.05 - 0.15

Hydraulic retention time: 18-24 hours
 F/M Ratio: Low
 Organism Growth Rate: net zero
 Sludge Age: Long
 Effluent Quality: Good

51

Typical ASP Loading Ranges

Loading Rate	Hydraulic Retention Time (hrs)	Sludge age (days)	Volumetric Loading (lb BOD/1000 ft ³)	F/M (lb/lb · day)
Low Rate	18-24	20 - 30	10 - 25	0.05 - 0.15
Conventional	6-8	5 - 15	20 - 40	0.2 - 0.5
High Rate	1-3	1 - 3	100 - 1,000	0.5 - 1.5

Source: Table 5.3 Operation of Wastewater Treatment Plants, Vol. 1 1st Edition, Water Programs Sacramento State

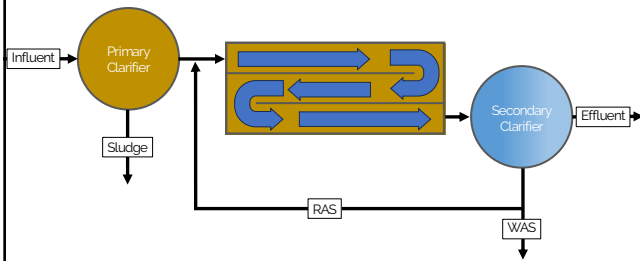
52

Complete Mix vs Plug Flow



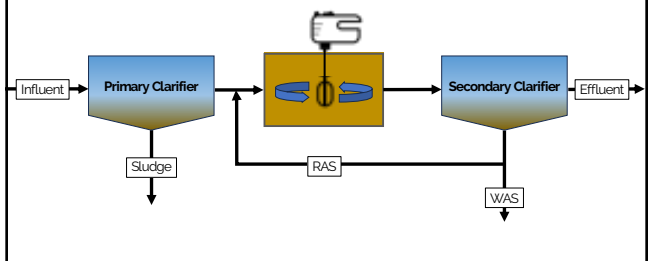
53

Plug Flow



54

Complete Mix



55

Oxidation Ditch (Combo)



56

Sludge Age

Sludge age, MCRT or Solids Retention Time
Average time solids are retained in the aeration tank

$$\text{Sludge Age (days)} = \frac{\text{mass of solids in tank}}{\text{mass rate of solids entering tank}}$$

$$\text{Sludge Age (days)} = \frac{V_{ab} \times MLSS}{Q \times TSS_{INF}} \quad \text{where } TSS_{INF} = \text{Total Suspended Solids in aeration tank influent}$$

57

Solids Retention Time

$$SRT(days) = \frac{[V_{ab} \times MLSS] + [V_{sc} \times TSS_{sc}]}{[Q_{WAS} \times TSS_{WAS}] + [Q_{eff} \times TSS_{eff}]}$$

TSS_{sc} = TSS in secondary clarifier
TSS_{eff} = TSS in secondary effluent
TSS_{WAS} = TSS in WAS

OR, if activated sludge is pumped out of the secondary clarifier promptly so that there are only minimum solids in the clarifier, the secondary clarifier term can be left out of the equation

$$SRT(days) = \frac{[V_{ab} \times MLSS]}{[Q_{WAS} \times TSS_{WAS}] + [Q_{eff} \times TSS_{eff}]}$$

58

Solids Retention Time

$$SRT(days) = \frac{[V_{ab} \times MLSS]}{[Q_{WAS} \times TSS_{WAS}] + [Q_{eff} \times TSS_{eff}]}$$

V_{ab} = 1 Mgal (MG)
Q = 4 Mgal/day (MGD)
Q_{WAS} = 0.075 Mgal/day (MGD)
MLSS = 2,400 mg/L
TSS_{WAS} = 6,200 mg/L
TSS_{eff} = 12 mg/L

$$Q_{eff} = Q - Q_{WAS}$$

59



60

Solids Retention Time

$$SRT(days) = \frac{[V_{ab} \times MLSS]}{[Q_{WAS} \times TSS_{WAS}] + [Q_{eff} \times TSS_{eff}]}$$

V_{ab} = 1 Mgal (MG)
Q = 4 Mgal/day (MGD)
Q_{WAS} = 0.075 Mgal/day (MGD)
MLSS = 2,400 mg/L
TSS_{WAS} = 6,200 mg/L
TSS_{eff} = 12 mg/L

$$Q_{eff} = Q - Q_{WAS} = 4 \text{ MGD} - 0.075 \text{ MGD} = 3.925 \text{ MGD}$$

$$SRT(days) = \frac{1 \text{ (MG)} \times 2,400 \text{ mg/L}}{[0.075 \text{ MGD} \times 6,200 \text{ mg/L}] + [3.925 \text{ MGD} \times 12 \text{ mg/L}]}$$

$$SRT(days) = 4.7 \text{ days}$$

61

Design Characteristics

Process Name	Reactor Type	SRT (days)	F/M (lb BOD/LB VSS · d)	Volumetric Loading (lb BOD/1000 ft ³ D)	MLSS (mg/L)	Total Detention Time (hrs)
High-Rate Aeration	CMAS or Plug Flow	0.5 - 2	1.5 - 2	75 - 150	500 - 1500	1 - 2
Conventional Plug Flow	Plug Flow	3 - 15	0.2 - 0.4	20 - 40	1000 - 3000	4-8
Extended Aeration	CMAS or Plug Flow	20 - 40	0.04 - 0.1	5 - 15	2000 - 4000	20 - 30
Oxidation Ditch	CMAS & Plug Flow	15 - 30	0.04 - 0.1	5 - 15	3000 - 5000	15 - 30

62



63

Variables Effecting Process

Collection Systems & Plant Operations

64

Collection System Variables

Wastewater typically comes from domestic, commercial and industrial sources. Diurnal, weekly, and seasonal changes in water use will impact wastewater flows from all three source types, but not necessarily equally or in step.

Wastewater characteristics can change as they move through the collection system due to pollutants and chemicals entering the system.

I & I in a sanitary sewer can increase wastewater flow into the plant during storm events

In a combined sewer system typically get increased flows during storm events and spring thaws which can cause hydraulic overload at the plant

Collection system blockages and maintenance events can lead to the release of large volumes of septic wastewater that may cause a shock load on treatment plant systems

65

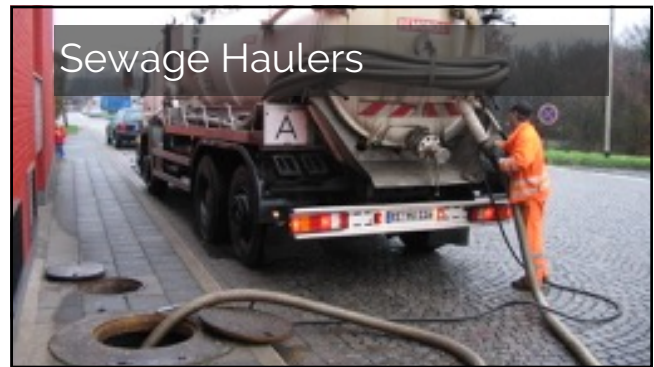
Plant Operational Variables

Changes in Influent characteristics (BOD, COD, TSS, VSS, TKN, Ammonia, Nitrate phosphorus, pH & alkalinity) will impact operation of an ASP.

Plants are designed with ranges in mind, so characteristics have to be monitored and processes have to be adjusted for changes.

Changes in internal recycle flows can also impact an ASP both in terms of flow and loading

66



67

Safety Considerations

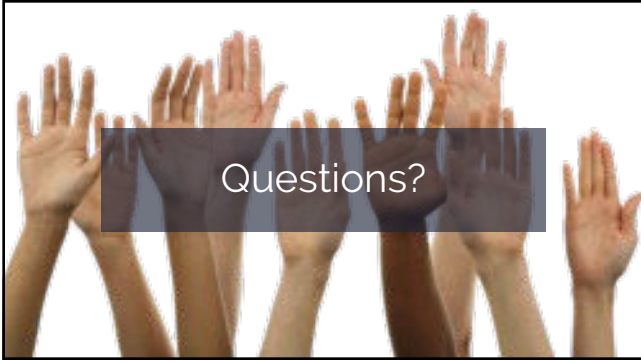
68

Typical Hazards

- Drowning – aeration reduces buoyancy
- Slippery edges
- Rotating equipment
- Electrical hazards
- Compressed air
- Biohazards
- Chemical hazards
- Noise
- Confined spaces



69



70



71

Office Hour Details

Time: Every Tuesday from: 9:00 AM to 10:00 AM PDT
10:00 AM to 11:00AM MDT
11:00 AM to Noon CDT
Noon to 1:00 PM EDT

Reach out via email: ajbarney1@unm.edu
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72

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73